

Project

CABLE BAND BOLT FACTOR OF SAFETY

Job Ref

Part of structure

CABLE BAND/HANGER LOADS

Calc sheet no rev

1

Drawing ref

3311/AB/20

Calc by

PS

Date

22/07/2011

Check by

Date

Ref

Calculations

Output

BS5400-2
2006

Footway HANGER LOADS

FOR LOADED LENGTHS IN EXCESS 36M $K \times 5.0 \text{ kN/m}^2$

CLAUSE 6.5.1.1

$$\frac{\text{Nominal HA UDL} \times 10}{L + 270} = K \quad L = \text{LOADED LENGTH}$$

Nominal HA UDL CLAUSE 6.2.3

CL 6.4.1

$$W = 36 \left(\frac{1}{L} \right)^{0.1} \text{ kN} \quad L = 1414 \text{ m} \quad (1)$$

$$W = 36 \left(\frac{1}{1414} \right)^{0.1} \text{ kN} \quad L = 326 \text{ m} \quad (2)$$

$$= 17.43 \text{ kN/Per Metre of LANE} \quad (1)$$

$$= 36 \left(\frac{1}{326} \right)^{0.1} = 20.183 \text{ kN Per M of LANE} \quad (2)$$

$$K = \frac{17.43 \times 10}{1414 + 270} = 0.117 \text{ kN} \quad (1)$$

$$K = \frac{20.183 \times 10}{326 + 270} = 0.339 \quad (2)$$

Footway Loading

$$\text{Uniformly Distributed Load} = 0.117 \times 5 = 0.585 \text{ kN/m}^2 \quad (1)$$

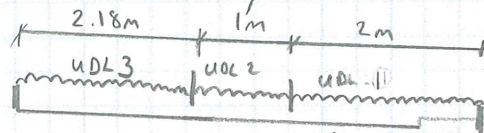
$$\text{UDL Loading} = 0.339 \times 5 \times 1.695 \text{ kN/m}^2 \quad (2)$$

CL 6.5.12

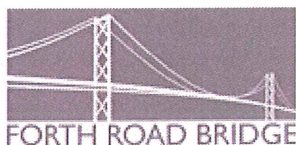
Intensities May Be Reduced By 15% Between 2-3m Width

" " " " By 30% Between 3-6m Width

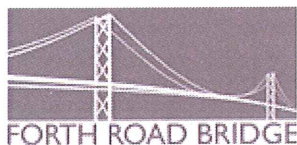
Total Width of Footway = 5.18m



Footway Elevation



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BS5400-2	<u>FOOTWAY LOADING (CONT)</u> <u>LOADED LENGTH ①</u> UDL 1 = 0.585 kN/m² UDL 2 = 0.497 kN/m² UDL 3 = 0.409 kN/m² CL 6.5.1.1 THESE INTENSITIES MAY BE AVERAGED OVER WIDTH $\therefore \frac{2}{5.18} \times 0.585 + \frac{1}{5.18} \times 0.497 + \frac{2.18}{5.18} \times 0.409$ $= 0.226 + 0.0959 + 0.172 = \underline{\underline{0.494 \text{ kN/m}^2}}$ <u>LOADED LENGTH ②</u> UDL 1 = 1.695 kN/m² UDL 2 = 1.44 kN/m² UDL 3 = 1.19 kN/m² $\therefore \frac{2}{5.18} \times 1.695 + \frac{1}{5.18} \times 1.44 + \frac{2.18}{5.18} \times 1.19$ $= 0.654 + 0.278 + 0.500 = \underline{\underline{1.433 \text{ kN/m}^2}}$ CL 6.5.1.2 WHERE A MAIN STRUCTURAL MEMBER SUPPORTS 2 OR MORE NOTATIONAL LANES OF TRAFFIC, THE FOOTWAY/CYCLE TRACK LOADING MAY BE FURTHER REDUCED SUCH THAT: ON FOOTWAYS 0.5 OF UDL ABOVE ON CYCLEWAY 0.2 OF UDL ABOVE <u>Assumption</u> ASSUME 2m OF WIDTH IS A FOOTWAY & REMAINDER IS A CYCLE WAY.	



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Footway Loading (Cont)

LOADED LENGTH ①

$$= \frac{2}{5.18} \times 0.494 \times 0.5 + \frac{3.18}{5.18} \times 0.414 \times 0.2$$

$$= 0.0953 + 0.061 = \underline{\underline{0.1563 \text{ kN/m}^2}}$$

LOADED LENGTH ②

$$= \frac{2}{5.18} \times 1.433 \times 0.5 + \frac{3.18}{5.18} \times 0.2 \times 1.433$$

$$= 0.28 + 0.176 = \underline{\underline{0.46 \text{ kN/m}^2}}$$

Footway Loading

$$= \underline{\underline{0.1563 \text{ kN/m}^2}}$$

$$= \underline{\underline{0.46 \text{ kN/m}^2}}$$

BRIDGE SPECIFIC LIVE LOAD

As stated in WAF BRIDGE SPECIFIC FOOTWAY LIVE LOADING REPORT MARCH 2006 RECOMMENDATIONS OF LOADINGS ARE GIVEN BELOW

$$\text{LOADED LENGTH 300m} = \underline{\underline{0.67 \text{ kN/m}}}$$

$$\text{LOADED LENGTH 1414m} = \underline{\underline{0.23 \text{ kN/m}}}$$

TOTAL LOAD APPLIED

①

$$\text{BD37/01 } 1414 \times 0.1563 \times 5.18 = \underline{\underline{1144.8 \text{ kN}}}$$

$$\text{BSFLL } 1414 \times 0.23 = \underline{\underline{325.2 \text{ kN}}}$$

②

$$\text{BD37/01 } 318 \times 0.46 \times 5.18 = \underline{\underline{757.7 \text{ kN}}}$$

$$\text{BSFLL } 318 \times 0.67 = \underline{\underline{213 \text{ kN}}}$$

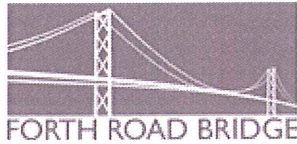
PER HANGER (Approx)

$$= \underline{\underline{15.3 \text{ kN}}}$$

$$= \underline{\underline{4.3 \text{ kN}}}$$

$$= \underline{\underline{45 \text{ kN}}}$$

$$= \underline{\underline{12.6 \text{ kN}}}$$



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CABLE BAND BOLT FAULTS & SAFETY

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NOMINAL AXIAL LOADS IN HANGER

AVERAGE AXIAL LOAD IN MAIN SPAN HANGER =

$$= 1470 \text{ kN PER HANGER USING BD37/01}$$

CALCULATE LOAD FOR HANGER USING BSFLL & LOADED LENGTH OF 1414

MAIN SPAN $L = 318 \text{ m}$

$$\text{HANGER LOAD} = 1470 - 45 + 12.6 = 1437.6 \text{ kN}$$

$$\text{AS A PERCENTAGE} = \frac{1437.6}{1470} \times 100 = 97.75\%$$

$\therefore$ LOAD DECREASE BY 3.2%

HANGER LOAD

$$= \underline{\underline{1437.6 \text{ kN}}}$$

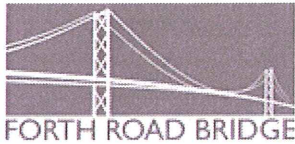
SIDE SPAN $L = 318 \text{ m}$

$$\text{HANGER LOAD} = 1955 - 45 + 12.6 = 1922.6 \text{ kN}$$

$$\text{AS A PERCENTAGE} = \frac{1922.6}{1955} \times 100 = 98.3\%$$

$\therefore$ LOAD DECREASES BY 1.66%

$$= \underline{\underline{1922.6 \text{ kN}}}$$



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CABLE BANDS

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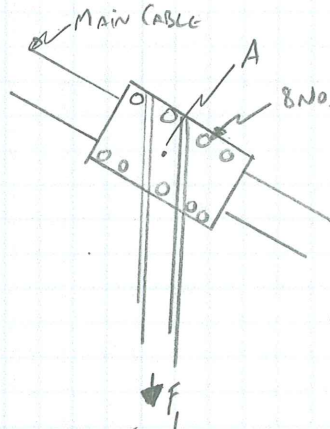
Ref

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DETERMINE FOS AGAINST SLIP

PANEL POINT 42



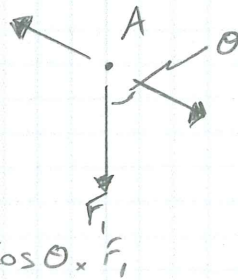
8 No. Cable Band Bolts

Bolt Tension = 800kN EACH.

$F_1 = 1920 \text{ kN DL+LL}$

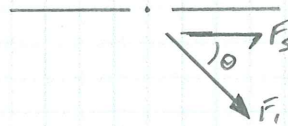
Assume Slip $\mu = 0.3$

IDEALISED DIAGRAM

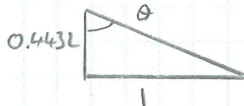


$$F_2 = \cos \theta \times F_1$$

FORCE CAUSING SLIP



DETERMINE θ SLOPE OF CABLE



$$\tan \theta = \frac{1}{0.4432} \Rightarrow \tan^{-1} \left(\frac{1}{0.4432} \right)$$

$$\theta = \underline{\underline{66.09^\circ}}$$

SLOPE = 66.09.

$$\begin{aligned} F_2 &= \cos 66.09^\circ \times 1920 \\ &= \underline{\underline{778.18 \text{ kN}}} \end{aligned}$$

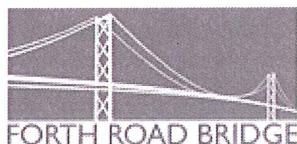
FORCE RESISTING SLIP

$$8 \text{ No Bolts} = 8 \times 800 \times 0.3 = \underline{\underline{1920 \text{ kN}}}$$

$$\text{FOS} = \frac{1920}{778.18} = \underline{\underline{2.46}} \quad \text{THEREFORE MB USED}$$

INCORRECT ANGLE

FROM TABLE
FOS 2.33



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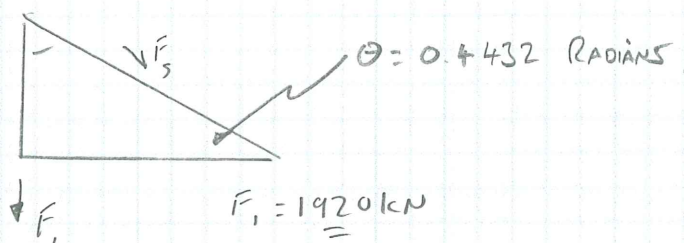
Date

Ref

Calculations

Output

Calculations As MB



$$F_s = \sin(0.4432) \times 1920 = \underline{\underline{823.4 \text{ kN}}}$$

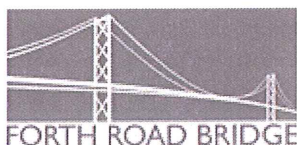
Force Resisting Slip

$$8 \text{ No. Bolts} = 8 \times 800 \times 0.3 = \underline{\underline{1920 \text{ kN}}}$$

$$\text{FOS} = \frac{1920}{823.4} = \underline{\underline{2.33}}$$

As stated using the slope as an angle in radians produces incorrect results.

As per MB
Calculation
Sheet.



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CABLE BANDS FRICTION

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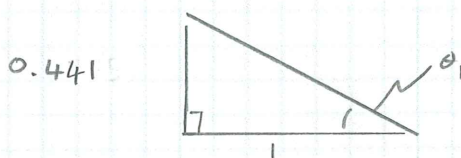
Calculations

Output

CHECK SLOPE CALCULATION

PANNEL POINT 42.

AS SLOPE DETERMINED FROM GRAPH OF
LWE OF CABLE SLOPE AT PP42:



$$\theta_1 = \tan^{-1} \left(\frac{0.441}{1} \right) = 23.79^\circ$$

CHECK SLOPE USING 2 POINTS ON CABLE

Survey
WAF
1986

Point S3 - Level - 153.6 N - 1993.714

Point S2 - Level - 146.251 N - 1977.574

$$\text{SLOPE} = \frac{153.6 - 146.251}{1993.714 - 1977.574} = \frac{7.349}{16.14} = 0.455$$

THEREFORE ANGLE IS CORRECT.



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CABLE BAND BOLT - FOS.

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CABLE BAND - Friction

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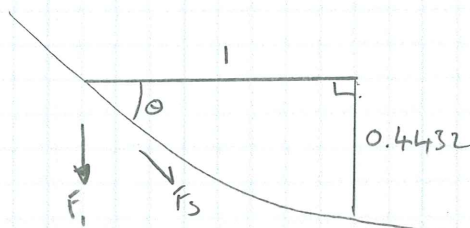
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CARRY OUT CALC USING RADIANS



$$\theta = \tan^{-1}(0.4432) = 0.417 \text{ RAD.}$$

$$\sin \theta = \frac{F_1}{F_S}$$

$$\therefore F_S = F_1 \sin \theta = 1920 \sin(0.417) \\ = \underline{\underline{774.7 \text{ kN}}}$$

$$\text{FOS} = \frac{1920}{774.7} = 2.47 \text{ FOS.}$$

using DEGREES = 2.46 FOS TURNING EQUAL AS EXPECTED.

USE DEGREES AS IT IS SLIGHTLY MORE CONSERVATIVE.